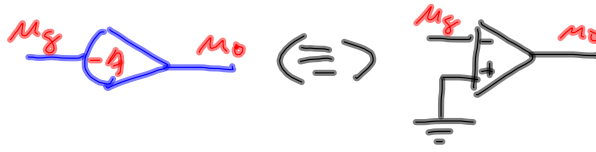


OPERATIONAL AMPLIFIER

IGL
25.12.2017

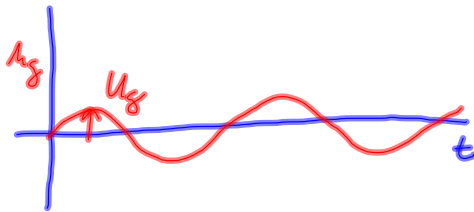


u_g ... INPUT VOLTAGE [V] $u_o = -A \cdot u_g$

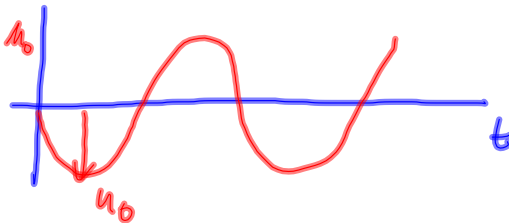
u_o ... OUTPUT VOLTAGE [V]

A ... GAIN

$(-A)$... CHANGE POLARITY



$$u_g = u_g \sin(\omega t)$$



$$u_o = -A u_g \sin(\omega t)$$

ABSOLUTE VALUE

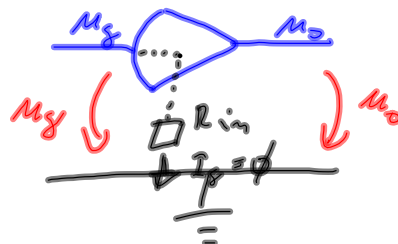
$$\text{GAIN} = \left| \frac{u_o}{u_g} \right| = A$$

IDEAL PROPERTIES

$$A = \infty$$

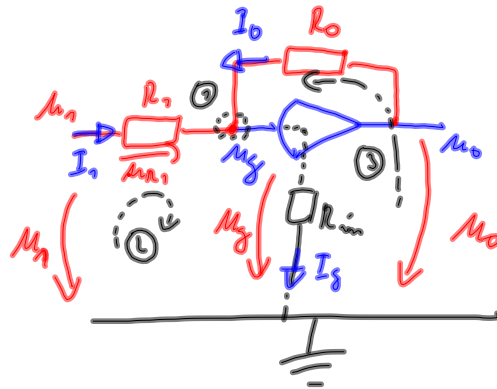
$$R_{in} = \infty [\Omega]$$

$$R_{out} = 0 [\Omega]$$



$A \rightarrow -\infty$... ONLY THEORETICAL

PRACTICAL APPLICATION WITH RESISTOR



QUESTIONS

$u_0 = f(u_1)$
??

I. KIR. LAW

① $I_1 + I_0 - I_g = \phi$

I. KIRCH. LAW

② $R_1 I_1 + u_2 - u_1 = \phi$

$I_1 = \frac{u_1 - u_2}{R_1}$

③ $R_0 I_0 + u_2 - u_3 = \phi$

$I_0 = \frac{u_3 - u_2}{R_0}$

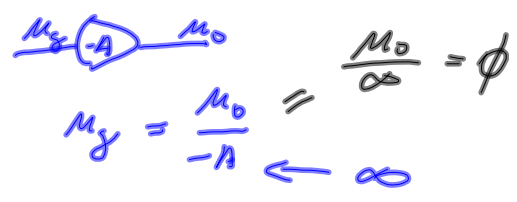


$I_g = \frac{u_2}{R_{in}}$

$u_2 = \phi$

PROPERTY OF OPEN. AMPLIF.

$u_0 = -A \cdot u_2$



$u_2 = \phi$!!

NOTE: $I_g = \frac{u_2}{R_{in}} = \frac{\phi}{\infty} = \phi$

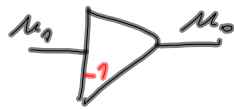
"VIRTUAL GND"

$$\frac{u_1 - u_s}{R_1} + \frac{u_o - u_s}{R_o} - \frac{u_s}{R_{in}} = \phi$$

$$\frac{M_1}{R_1} + \frac{M_o}{R_o} = \phi$$

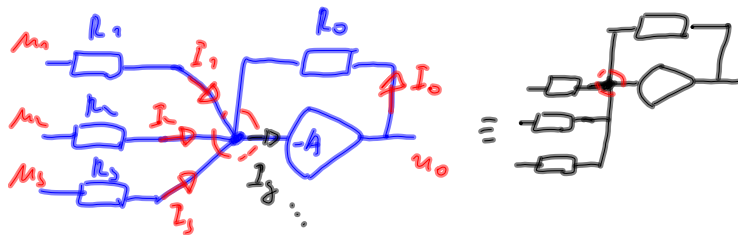
$$M_o = -M_1 \cdot \frac{R_o}{R_1}$$

1) INVERTER ($R_o = R_1$)



$$M_o = -M_1$$

2) INVERTING SUMMER



"VIRTHAL" $\rightarrow R_o$

$$I_1 + I_2 + I_3 - I_s = \phi$$

$$u_o = f(u_1, u_2, u_3)$$

$$\frac{M_1}{R_1} + \frac{M_2}{R_2} + \frac{M_3}{R_3} + \frac{M_o}{R_o} = \phi$$

$$M_o = - \left(\frac{R_o}{R_1} M_1 + \frac{R_o}{R_2} M_2 + \frac{R_o}{R_3} M_3 \right)$$

INVERTING

SUMMER

SPECIAL CASE ($R_o = R_1 = R_2 = R_3$) SUMMER



→ WHAT HAPPENS IF:

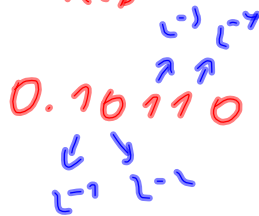
$$\begin{aligned}
 R_1 &= 2R_0 & \text{AND } u_1 &= u_2 = u_3 = \dots = u_n \\
 R_2 &= 4R_0 & & \parallel \\
 R_3 &= 8R_0 & & U_{REF} \\
 & \vdots & & \text{EG. } -1V \\
 R_i &= 2^i R_0 & \dots \text{ THEN} & \\
 & & u_o &= - \left(\frac{R_0}{2R_0} U_{REF} + \frac{R_0}{4R_0} U_{REF} + \dots \right)
 \end{aligned}$$

$$u_o = + \left(\frac{1}{2} + \frac{1}{4} + \frac{1}{8} + \dots + \frac{1}{2^i} \right)$$

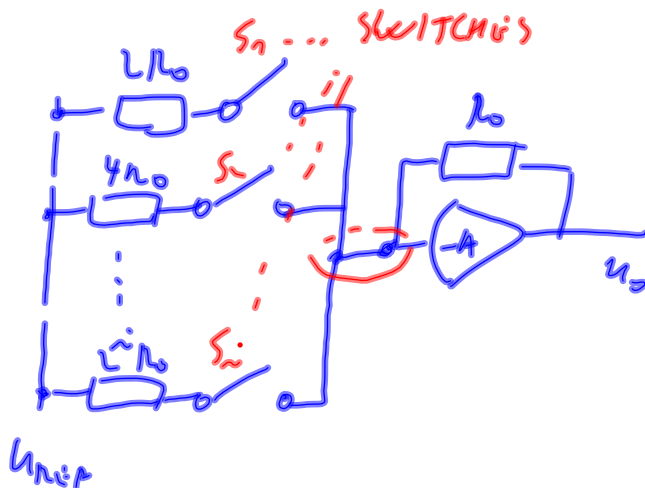
\parallel \parallel \parallel \parallel
 2^{-1} 2^{-2} 2^{-3} 2^{-i}

BINARY REPRESENTATION OF

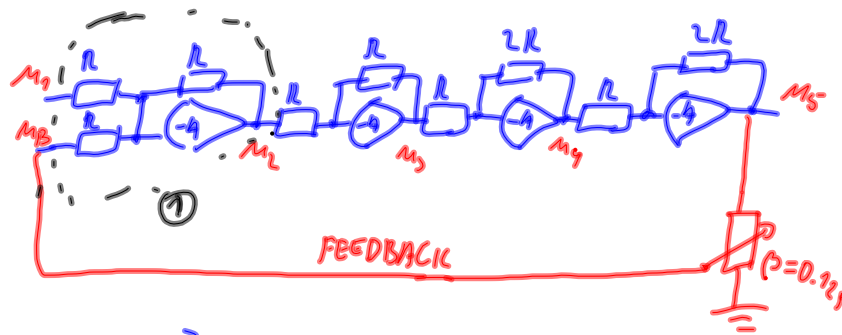
"NORMALIZED" NUMBER (< 1)



⇒ USAGE IN D/A, A/D CONVERTERS



EX ANALYZE CIRCUIT WITH O.A.



$A = -\infty$, $\beta = 0.125$, $M_1 = 0.3V$, $R = 1000\Omega$
 NOT NEGATIVE
 $M_B = \beta \cdot M_5$

→ COMPUTE $M_5 = f(M_1)$ ∴

$M_2 = - \left(M_1 \frac{R}{R} + M_B \frac{R}{R} \right) \dots$ ① INVERTING SUMMATION
 $\beta \cdot M_5$

$M_3 = -M_2 \frac{R}{R} \dots$ INVERSION

$M_4 = -M_3 \frac{2R}{R} \dots$ AMPLIFIERS

$M_5 = -M_4 \frac{2R}{R}$

SUBSTITUTE: $M_3 = -M_2 = M_1 + \beta M_5$

$M_4 = -2M_3 = -2(M_1 + \beta M_5)$

$M_5 = -2M_4 = -2(-2(M_1 + \beta M_5)) =$
 $= 4M_1 + 4\beta M_5$

$M_5 = \frac{4}{1-4\beta} \cdot M_1 = \underline{\underline{8M_1}}$
 $\beta = 0.125$

NOTE: $\beta \neq \frac{1}{4}$

SUMMARY ELE

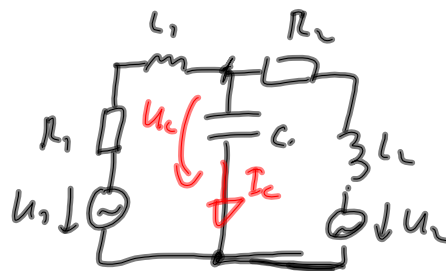
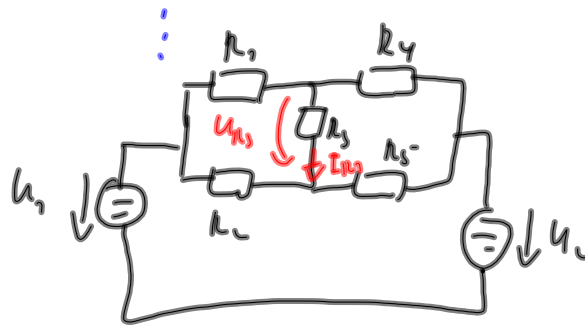
→ SOLUTION OF "LINEAR" CIRCUITS

R, L, C

(AC / DC)

↓
STEADY STATE
COMPLEX NUMBERS

- METHOD OF SUPERPOSITION
- LOOP CURRENT METHOD
- NODE VOLTAGE METHOD
- THEVENIN'S THEOREM



THEVENIN'S
THEOREM

→ SOLUTION OF "NON-LINEAR" GL. CIRC.

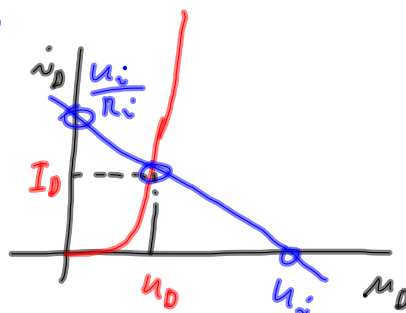
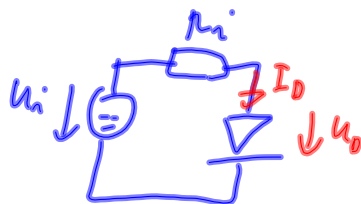
(GRAPHICAL SOLUTION)

DIODES, TRANSISTORS

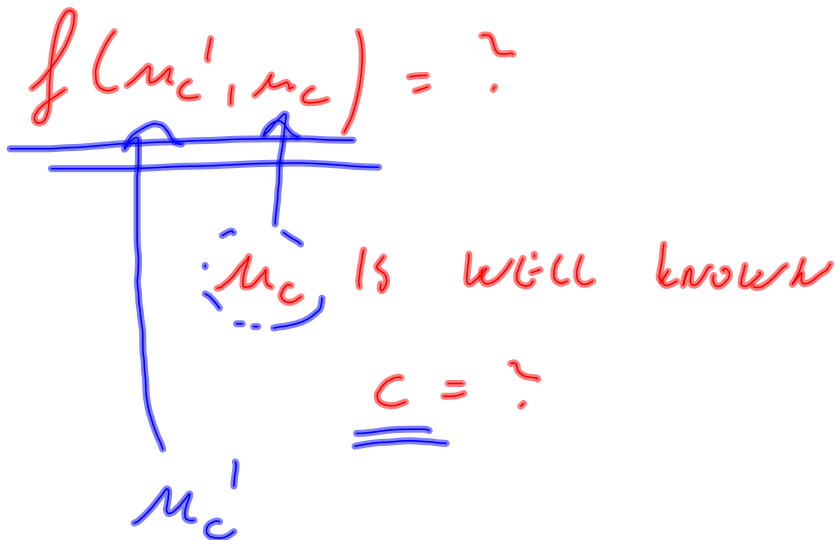
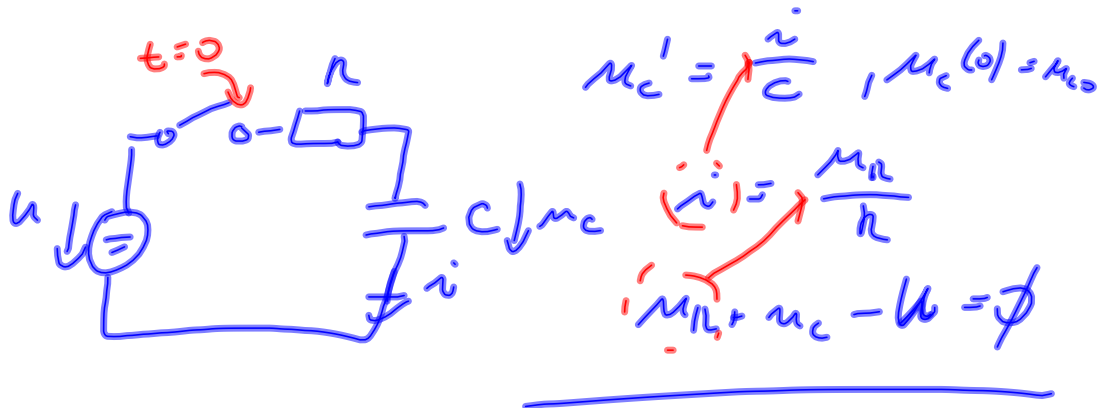
PN JUNCTIONS

→ GAIN

THEVENIN'S THEOREM



→ TRANSIENT STATES IN RLC
CIRCUITS (DIFFERENTIAL EQUATIONS)



→ + OPERATIONAL AMPLIFIERS